

1. NaF(s) 증발

$$\ln P(\text{atm}) = \frac{-34450}{T} - 2.01 \ln T + 33.74$$

NaF(l) 증발

$$\ln P(\text{atm}) = \frac{-31090}{T} - 2.52 \ln T + 34.66$$

(a) normal boiling temperature-?

$$\ln 1 = \frac{-31090}{T} - 2.52 \ln T + 34.66$$

$$T = 2006.1 \text{ K}$$

(b) 삼중점의 T, P는?

$$\frac{-34450}{T} - 2.01 \ln T + 33.74 = \frac{-31090}{T} - 2.52 \ln T + 34.66$$

$$\frac{-3360}{T} + 0.51 \ln T - 0.92 = 0$$

$$T = 1238.9 \text{ K}$$

이를 대입하면,

$$P = 2.289 \times 10^{-4} \text{ atm.}$$

(c) normal boiling T 에서 molar 증발열은?

$$d \ln P = \frac{\Delta H}{RT^2} dT$$

$$\frac{d \ln P}{dT} = \frac{31090}{T^2} - \frac{2.52}{T} = \frac{\Delta H_{\text{evap.}}}{RT^2}$$

$$\Delta H_{\text{evap.}} = R(31090 - 2.52T)$$

normal boiling T 2006.1 K, R = 8.31446 J/K·mol 이서,

$$\Delta H_{\text{evap.}} = 216464 \text{ J/mol}$$

$$= 216.5 \text{ kJ/mol}$$

(d) 삼중점까지 molar 용해열은?

$$\Delta H^{s \rightarrow l} = \Delta H^{s \rightarrow g} + \Delta H^{g \rightarrow l}$$

$$= \Delta H^{s \rightarrow g} - \Delta H^{l \rightarrow g}$$

$$= R(34450 - 2.01 T) - R(31090 - 2.52 T)$$

$T = 1238.9 \text{ K}$ 를 대입하면, (삼중점 T)

$$\Delta H^{s \rightarrow l} = 33190 \text{ J/mol}$$

$$= \boxed{33.19 \text{ kJ/mol}}$$

(e) $\text{NaF}(l)$, $\text{NaF}(s)$ 의 C_p 값은?

$$\frac{dH}{dT} = C_p$$

$$\Delta C_p^{s \rightarrow l} = \frac{d\Delta H^{s \rightarrow l}}{dT} = \frac{dR(34450 - 31090 + 0.51 T)}{dT}$$

$$= 0.51 R$$

$$= \boxed{4.24 \text{ J/mol} \cdot \text{K}}$$

또는, $\ln P = \left[* \right] \frac{1}{T} + \frac{\Delta C_p}{R} \ln T + \text{constant}$ 에서,

$$\frac{\Delta C_p^{s \rightarrow v}}{R} = -2.01, \quad \frac{\Delta C_p^{l \rightarrow v}}{R} = -2.52 \text{ 에서,}$$

$$\Delta C_p^{s \rightarrow l} = 0.51 R.$$

2. $\frac{4\pi}{3} r^3$ 구의 부피 $P = \frac{2\sigma}{r}$

$$dG^S = -S^S dT + V_m d\frac{2\gamma_s}{r}$$

$$dG^L = -S^L dT + V_m d\frac{2\gamma_L}{r}$$

$$dG^S = dG^L \text{ at } T, \left(\frac{4\pi}{3} r^3\right)$$

$$\Delta S_m dT = V_m \left(d\frac{2\gamma_L}{r} - d\frac{2\gamma_s}{r} \right)$$

$$-\frac{\Delta H_m}{T_m} dT = 2V_m (\gamma_s - \gamma_L) d\frac{1}{r}$$

$$r \rightarrow \infty \text{ (bulk) 일 때 } T = T_m, \quad r = r \text{ (nano) 일 때 } T = T_m'$$

$$\int_{T_m}^{T_m'} -\frac{\Delta H_m}{T_m} dT = \int_{\infty}^r 2V_m (\gamma_s - \gamma_L) d\frac{1}{r}$$

$$\frac{\Delta H_m}{T_m} \Delta T_m = 2V_m (\gamma_s - \gamma_L) \frac{1}{r} \quad (\Delta T_m = T_m - T_m')$$

$$\therefore \frac{\Delta T_m}{T_m} = \frac{\gamma_s - \gamma_L}{\Delta H_m} \cdot \frac{2}{r} V_m$$

3. subregular soln model, A-B 2nd soln.

(a) partial molar G ?

$$G = x_A \bar{G}_A + x_B \bar{G}_B \Rightarrow dG = \bar{G}_A dx_A + \bar{G}_B dx_B$$

$$\frac{dG}{dx_B} = -\bar{G}_A + \bar{G}_B \quad (\because x_A = 1 - x_B)$$

$$(1 - x_B) \frac{dG}{dx_B} = -\bar{G}_A x_A + \bar{G}_B x_A$$

$$+ \left| G = x_A \bar{G}_A + x_B \bar{G}_B \right.$$

$$G + (1 - x_B) \frac{dG}{dx_B} = \bar{G}_B$$

$$\therefore \begin{cases} \bar{G}_A = G_m + (1 - x_A) \frac{dG_m}{dx_A} \\ \bar{G}_B = G_m + (1 - x_B) \frac{dG_m}{dx_B} \end{cases}$$

$$\bar{G}_A = G_m + (1 - x_A) \left({}^\circ G_A - {}^\circ G_B + RT(\ln x_A + 1 - \ln x_B - 1) + 6L_1 x_A x_B - L_0(x_A - x_B) - L_1 \right)$$

$$= \cancel{x_A} {}^\circ G_A + \cancel{x_B} {}^\circ G_B + RT \{ x_A \ln x_A + x_B \ln x_B \} + x_A x_B \{ L_0 + (x_A - x_B) L_1 \} + (1 - x_A) {}^\circ G_A - x_B {}^\circ G_B + RT(\ln x_A - \ln x_B) x_B + 6L_1 x_A x_B^2 - L_0 x_B(x_A - x_B) - L_1 x_B$$

$$= {}^\circ G_A + RT \ln x_A + L_0 x_B^2 + L_1 x_B(x_A^2 + 5x_A x_B - 1)$$

$$= \underline{{}^\circ G_A + RT \ln x_A + L_0 x_B^2 + L_1 x_B^2(4x_A - 1)}$$

같은 방법으로,

$$\underline{\bar{G}_B = {}^\circ G_B + RT \ln x_B + L_0 x_A^2 + L_1 x_A^2(1 - 4x_B)}$$

$$\begin{aligned}
 (b) \quad \Delta \overline{G}_A^{XS} &= L_0 x_B^2 + L_1 x_B^2 (4x_A - 1) \\
 &= (1-x_A)^2 (L_0 + L_1 (4x_A - 1)) \\
 &= RT \ln \gamma_A.
 \end{aligned}$$

$$\lim_{x_A \rightarrow 0} \Delta \overline{G}_A^{XS} = L_0 - L_1 = \lim_{x_A \rightarrow 0} RT \ln \gamma_A \neq 0.$$

(constant)

$\therefore x_A \rightarrow 0$ 이면 $\gamma_A = \text{constant} \neq 1 \Rightarrow$ Henryan 기동 만족

$$\lim_{x_A \rightarrow 1} \Delta \overline{G}_A^{XS} = 0 = \lim_{x_A \rightarrow 1} RT \ln \gamma_A$$

$\therefore x_A \rightarrow 1$ 이면 $\gamma_A = 1 \Rightarrow$ Raoultian 기동 만족.

B 이션도 마찬가지로,

$$\Delta \overline{G}_B^{XS} = (1-x_B)^2 (L_0 + L_1 (1-4x_B)) = RT \ln \gamma_B.$$

$$| x_B \rightarrow 0 \text{ 이면 } \Delta \overline{G}_B^{XS} = L_0 + L_1 = \text{constant} = RT \ln \gamma_B \neq 0.$$

$\therefore \gamma_B = \text{constant} \neq 1 \Rightarrow$ Henryan 기동 만족.

$$x_B \rightarrow 1 \text{ 이면 } \Delta \overline{G}_B^{XS} = 0 = RT \ln \gamma_B$$

$\therefore \gamma_B = 1 \Rightarrow$ Raoultian 기동 만족.

(c) $\bar{G}_A$, Gibbs-Duhem eqn ($\sum_{k=1}^C x_k d\bar{Q}_k = 0$) $A_B \rightarrow \bar{G}_B$ in Σ .

$$\begin{cases} \bar{G}_A = {}^0G_A + RT \ln x_A + L_0 x_B^2 + L_1 x_B^2 (4x_A - 1) \\ x_A d\bar{G}_A + x_B d\bar{G}_B = 0 \Rightarrow x_A \frac{d\bar{G}_A}{dx_A} + x_B \frac{d\bar{G}_B}{dx_A} = 0. \end{cases}$$

$$\frac{d\bar{G}_A}{dx_A} = \frac{RT}{x_A} + 2(x_A - 1)L_0 + L_1 \cdot 2(x_A - 1)(4x_A - 1) + L_1 \cdot 4x_B^2$$

$$= \frac{RT}{x_A} - 2x_B L_0 + L_1 x_B (-4x_A + 1 + 2x_B)$$

$$x_A \frac{d\bar{G}_A}{dx_A} = RT - 2x_A x_B L_0 - 6L_1 x_A x_B (x_A - x_B)$$

$$x_A d\bar{G}_A + x_B d\bar{G}_B = 0 \text{ 에서,}$$

$$x_B \frac{d\bar{G}_B}{dx_A} = -RT + 2x_A x_B L_0 + 6L_1 x_A x_B (x_A - x_B)$$

각 항을 나누어 보면, $\bar{G}_B$ 는,

$$\begin{aligned} \textcircled{1} \text{첫째 항: } \int -\frac{RT}{x_B} dx_A &= \int \frac{RT}{x_A - 1} dx_A = RT \ln |x_A - 1| + C \\ &= RT \ln x_B + C. \end{aligned}$$

$$\textcircled{2} \text{둘째 항: } \int 2L_0 x_A dx_A = L_0 x_A^2 + C.$$

$$\begin{aligned} \textcircled{3} \text{셋째 항: } \int 6L_1 x_A (x_A - x_B) dx_A &= 6L_1 \left(\frac{2}{3} x^3 - \frac{1}{2} x^2 \right) + C \\ &= L_1 (4x_A^3 - 3x_A^2) + C. \\ &= L_1 x_A^2 (1 - 4x_B) + C. \end{aligned}$$

$$\therefore \bar{G}_B = RT \ln x_B + L_0 x_A^2 + L_1 x_A^2 (1 - 4x_B) + C.$$

적분상수 C 를 0G_B 라 하면,

$$\bar{G}_B = {}^0G_B + RT \ln x_B + L_0 x_A^2 + L_1 x_A^2 (1 - 4x_B)$$

5. 1273K

$$G_m = \begin{cases} X_A G_A + X_B G_B + RT(X_A \ln X_A + X_B \ln X_B) & (\text{ideal}) \\ \quad " \quad \quad \quad " & + X_A X_B L_0 \quad (\text{regular}) \\ \quad " \quad \quad \quad " & + X_A X_B (L_0 + (X_A - X_B)L_1) \quad (\text{subregular}) \end{cases}$$

i) ideal opamp, $x_B = a_B$.

ii) regular 0102 ,

$$(x_B, a_{13}) = (0.10, 0.0320) \text{ OK!}$$

$$RT \ln a_B = RT \ln x_B + L_0 x_A^2$$

$$L_0 = \frac{RT(\ln a_B - \ln x_B)}{(1-x_B)^2} = -14889$$

$$\therefore a_B = \exp(\ln x_B - \frac{14889}{RT} (1-x_B)^2)$$

iii) subregular 이면,

$$RT \ln a_B = RT \ln x_B + L_0 x_A^2 + L_1 x_A^2 (1 - 4x_B)$$

$$(x_B, d_B) = (0.10, 0.0320), (0.20, 0.0800) \text{ 等}$$

$$L_0 + L_1(1 - 4x_R) = \frac{RT(\ln a_B - \ln x_B)}{(1 - x_B)^2}$$

$$L_0 + 0.6L_1 = -14889$$

$$L_0 + 0.2L_1 = -15154.$$

$$0.4L_1 = 264$$

$$L_1 = 662.5, \quad L_0 = -15286.5.$$

$$\therefore a_B = \exp\left(\ln x_B - \frac{15286.5}{RT} x_A^2 + \frac{662.5}{RT} x_A^2 (1 - 4x_B)\right)$$

이들 개념으로 어떤 아벨과 같고, 따라서 regular 일 때 가장 정교했다.

($\mathbb{Z}_7$: ideal, $\mathbb{Z}_{10}$: regular, $\mathbb{Z}_{15}$: subregular)

표로 나타내면 다음과 같다.

	ideal	regular	subregular	실제
0.10	0.1000	0.0320	0.0320	0.0320
0.20	0.2	0.0829	0.0800	0.0800
0.30	0.3	0.1506	0.1469	0.1492
0.40	0.4	0.2411	0.2346	0.2400
0.50	0.5	0.3518	0.3431	0.3510
0.60	0.6	0.4791	0.4696	0.4782
0.70	0.7	0.6168	0.6085	0.6162
0.80	0.8	0.7562	0.7509	0.7559
0.90	0.9	0.8894	0.8857	0.8874
1.00	1.0	1.0000	1.0000	1.0000

regular가 실제값과 가장 비슷하다.

6. ternary phase diagram

