

1.

$$(a) p_g = 1 \quad \therefore 0 = -\frac{31090}{T} - 2.52 \ln T + 34.66 \quad \therefore T_b = 2006 \text{ K}$$

$$(b) p_s = p_g = p_g \quad p_s = p_g$$

$$\Rightarrow -\frac{34450}{T} - 2.01 \ln T + 33.74 = -\frac{31090}{T} - 2.52 \ln T + 34.66 \quad \Rightarrow T = 1239 \text{ K}$$

$$(c) d(\ln p) / dT = \Delta H / RT^2 \Rightarrow 31090 \cdot \frac{1}{T^2} - \frac{2.52}{T} = \frac{\Delta H}{RT^2} \Rightarrow \Delta H = 216.5 \text{ kJ/mol}$$

$$(T = 2006 \text{ K})$$

$$(d) \Delta H_{H_2} = \Delta H_{H_2g} - \Delta H_{H_2g} \quad \Rightarrow \Delta H_{H_2g} = R [34450 - 2.01T], \Delta H_{H_2g} = R [31090 - 2.52R], T = 1239 \text{ K}$$

$$\Rightarrow \Delta H_{H_2g} = 265.7 \text{ kJ/mol}, \Delta H_{H_2g} = 232.5 \text{ kJ/mol}$$

$$\therefore \Delta H_{H_2} = 33.2 \text{ kJ/mol}$$

$$(e) \Delta C_p = d(\Delta H_{H_2}) / dT = d(\Delta H_{H_2g}) / dT - d(\Delta H_{H_2g}) / dT = -2.01R + 2.52R = 4.24 \text{ J/K}$$

2.

$$l \rightarrow s \quad \Delta p = \frac{2}{r} (\gamma_s - \gamma_l) \quad \frac{dp}{dT} = \frac{\Delta H_m}{T \Delta V_m} \Rightarrow \frac{\Delta T_m}{T_m} = \frac{\Delta V_m}{\Delta H_m} \cdot p = \frac{2}{r} (\gamma_s - \gamma_l) \cdot \frac{\Delta V_m}{\Delta H_m}$$

3.

$$(a) \frac{\partial G_m}{\partial x_B} = -G_A + G_B + RT \{ \ln x_B - \ln x_A \} + (x_A - x_B) \{ L_0 + (x_A - x_B) L_1 \} - 2x_A x_B L_1$$

$$\frac{\partial G_m}{\partial x_A} = G_A - G_B + RT \{ \ln x_A - \ln x_B \} + (x_B - x_A) \{ L_0 + (x_A - x_B) L_1 \} + 2x_A x_B L_1$$

$$\bar{G}_B = G_m + (1 - x_B) \frac{\partial G_m}{\partial x_B} = {}^0G_B + RT \ln x_B + (1 - x_B)^2 \{ L_0 + (1 - 4x_B) L_1 \}$$

$$\bar{G}_A = G_m + (1 - x_A) \frac{\partial G_m}{\partial x_A} = {}^0G_A + RT \ln x_A + (1 - x_A)^2 \{ L_0 + (4x_A - 1) L_1 \}$$

(b)

$$i) x_A \gg x_B \quad \bar{G}_A = {}^0G_A + RT \ln x_A = {}^0G_A + RT \ln a_A \quad \therefore \lim_{x_A \rightarrow 1} a_A = x_A$$

$$\bar{G}_B = {}^0G_B + RT \ln x_B + (L_0 + L_1) = {}^0G_B + RT \ln a_B \quad \therefore \lim_{x_B \rightarrow 0} a_B = \exp\left(\frac{L_0 + L_1}{RT}\right) x_B = r_B^0 x_B$$

$$ii) x_A \ll x_B \quad \bar{G}_A = {}^0G_A + RT \ln x_A + (L_0 - L_1) = {}^0G_A + RT \ln a_A \quad \therefore \lim_{x_A \rightarrow 0} a_A = \exp\left(\frac{L_0 - L_1}{RT}\right) x_A = r_A^0 x_A$$

$$\bar{G}_B = {}^0G_B + RT \ln x_B = {}^0G_B + RT \ln a_B \quad \therefore \lim_{x_B \rightarrow 1} a_B = x_B$$

$$(c) x_A d\bar{G}_A + x_B d\bar{G}_B = 0 \Rightarrow d\bar{G}_B = -\frac{x_A}{x_B} d\bar{G}_A = -\frac{x_A}{x_B} \cdot \left(\frac{RT}{x_A} - 2(1 - x_A) \{ L_0 + (4x_A - 1) L_1 \} + 4(1 - x_A)^2 L_1 \right)$$

$$= -\frac{RT}{x_B} + 2x_A \{ L_0 + (4x_A - 1) L_1 \} - 4x_A (1 - x_A) L_1$$

$$\therefore \bar{G}_B = \int d\bar{G}_B = RT \ln x_B + x_A^2 L_0 + 4x_A^3 L_1 - 3x_A^2 L_1$$

$$= G_B^0 + RT \ln x_B + (1 - x_B)^2 \{ L_0 + (1 - 4x_B) L_1 \}$$

4.

(a) : liquid A, solid B

(h) : liquid A, liquid B

$$i) (a) \Delta G_L^M = RT(\chi_A \ln \chi_A + \chi_B \ln \chi_B) + L_{AB}(l) \chi_A \chi_B + (G_B^o(l) - G_B^o(s)) \chi_B$$

$$\Delta G_S^M = RT(\chi_A \ln \chi_A + \chi_B \ln \chi_B) + L_{AB}(s) \chi_A \chi_B + (G_A^o(s) - G_A^o(l)) \chi_A$$

$$\partial(\Delta G_L^M) / \partial \chi_B = \partial(\Delta G_S^M) / \partial \chi_B \Rightarrow \partial(\Delta G_L^M - \Delta G_S^M) / \partial \chi_B = 0$$

$$\Rightarrow \{ (G_B^o(l) - G_B^o(s)) + L_{AB}(l) \chi_A \} - \{ (G_A^o(l) - G_A^o(s)) + L_{AB}(s) \chi_A \} = 0$$

$$ii) (b) \Delta G_L^M = RT(\chi_A \ln \chi_A + \chi_B \ln \chi_B) + L_{AB}(l) \chi_A \chi_B$$

$$\Delta G_S^M = RT(\chi_A \ln \chi_A + \chi_B \ln \chi_B) + L_{AB}(s) \chi_A \chi_B + (G_A^o(s) - G_A^o(l)) \chi_A + (G_B^o(s) - G_B^o(l)) \chi_B$$

$$\Rightarrow \partial(\Delta G_L^M - \Delta G_S^M) / \partial \chi_B = 0$$

$$\Rightarrow \{ L_{AB}(l) \chi_A \} - \{ L_{AB}(s) \chi_A + (G_A^o(l) - G_A^o(s)) + (G_B^o(s) - G_B^o(l)) \} = 0$$

(a) 와 (b)의식의 평형이 되기 위해 만족해야 하는 식이 같다.

다라서 상평형 조건은 reference state에 상관없이 unique 하다.

5.

i) ideal solution : $\gamma_B \neq a_B$ 이므로 ideal 하지 않다.

ii) regular solution : $\Delta G^M = RT(\gamma_A \ln a_A + \gamma_B \ln a_B) = RT(\gamma_A \ln \gamma_A + \gamma_B \ln \gamma_B) + \gamma_A \gamma_B \Omega_{AB}$

$$\gamma_A \gamma_B \Omega_{AB} = RT(\gamma_A \ln \gamma_A + \gamma_B \ln \gamma_B)$$

$$\gamma_A \gamma_B \Omega_{AB} = \gamma_A \gamma_B^2 \Omega_{AB} + RT \gamma_B \ln \gamma_B$$

$$\gamma_A \Omega_{AB} = \gamma_A \gamma_B \Omega_{AB} + RT \ln \gamma_B$$

$$\Omega_{AB} = RT \ln \gamma_B / (1 - \gamma_B)^2 \Rightarrow \text{regular model 이터 상수}$$

γ_B	a_B	γ_B	Ω_{AB}
0.1	0.032	0.32	-14888.2
0.2	0.08	0.4	-15152.8
0.3	0.1498	0.499333	-15000.4
0.4	0.24	0.6	-15017.9
0.5	0.351	0.702	-14979
0.6	0.4782	0.797	-15009.1
0.7	0.6162	0.880286	-14994.6
0.8	0.7559	0.944875	-15003.1
0.9	0.8874	0.986	-14921.9
1	1	1	

$\Rightarrow \Omega_{AB}$ 가 -15000 으로 거의 일정

\therefore regular solution model 이 가장 적합

iii) sub regular solution model : Ω_{AB} 가 γ_B 에 따라 달라지지만, 실험 데이터에서 Ω 는 거의 일정하다. 따라서 복잡함

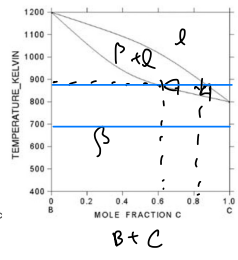
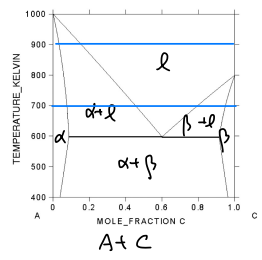
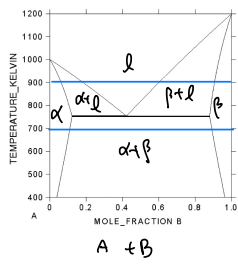
$$\begin{aligned} \Rightarrow \Delta G^M &= RT(\gamma_A \ln \gamma_A + \gamma_B \ln \gamma_B) + \gamma_A \gamma_B \Omega_{AB} \\ &= RT \left\{ (1 - \gamma_B) \ln (1 - \gamma_B) + \gamma_B \ln \gamma_B \right\} + (1 - \gamma_B) \gamma_B \cdot \frac{RT \ln \gamma_B}{(1 - \gamma_B)^2} \end{aligned}$$

$$RT \ln \gamma_B = \Omega_{AB} (1 - \gamma_B)^2 = \Omega_{AB} \gamma_A^2 \Rightarrow \gamma_B = \exp(\Omega_{AB} \cdot \gamma_A^2 / RT)$$

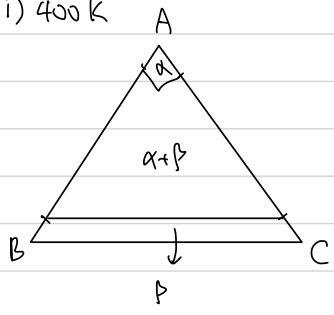
$\Rightarrow a_B = \gamma_B \exp(\Omega_{AB} \gamma_A^2 / RT)$. Ω_{AB} 는 평균값인 -14951.9 사용

γ_B	γ_A	a_B	Ω_{AB}	$a_B(0\%)$	오차
0.1	0.9	0.032	-14488.2	0.031844	0.486198
0.2	0.8	0.08	-15152.8	0.080978	-1.22201
0.3	0.7	0.1498	-15000.4	0.150137	-0.22482
0.4	0.6	0.24	-15017.9	0.240539	-0.22468
0.5	0.5	0.351	-14979	0.351225	-0.06406
0.6	0.4	0.4782	-15009.1	0.478614	-0.08648
0.7	0.3	0.6162	-14994.6	0.616424	-0.03635
0.8	0.2	0.7559	-15003.1	0.756046	-0.01936
0.9	0.1	0.8874	-14921.9	0.887375	0.002834
1	0	1	-14951.9		

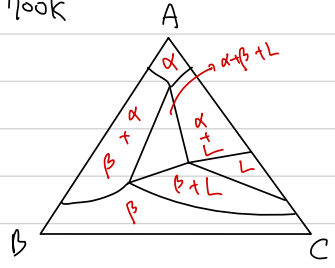
6.



i) 400 K



ii) 700 K



iii) 900 K

