

1. Vapor pressure of solid: $\ln p = -\frac{34450}{T} - 2.01 \ln T + 33.74$

Vapor pressure of liquid: $\ln p = -\frac{31090}{T} - 2.52 \ln T + 34.66$

a) boiling T: Vapor pressure = 1 atm $\frac{1}{\text{atm}}$ 온도

$$\ln 1 = 0 = -\frac{31090}{T} - 2.52 \ln T + 34.66$$

$$T_b = 2006 \text{ K}$$

b) T, P at the triple point

$$-\frac{34450}{T} - 2.01 \ln T + 33.74 = -\frac{31090}{T} - 2.52 \ln T + 34.66$$

$$\frac{3360}{T} - 0.51 \ln T + 0.88 = 0$$

$$T_{\text{triple}} = 1239 \text{ K}$$

(c) Molar heat of evaporation at boiling T

$$\ln p = -\frac{31090}{T} - 2.52 \ln T + 34.66$$

$$\frac{d \ln p}{dT} = \frac{\Delta H}{RT^2} = \frac{31090}{T^2} - \frac{2.52}{T}$$

$$\Delta H = 31090 R - 2.52 R T$$

$$T = 2006 \text{ K}$$

$$\Delta H_{\text{L} \rightarrow \text{V}} = 31090 \times 8.314 - 2.52 \times 8.314 \times 2006 = 216454 \text{ J}$$

d) molar heat of melting at triple point

$$\ln p = -\frac{34450}{T} - 2.01 \ln T + 33.74$$

$$\frac{d \ln p}{dT} = \frac{\Delta H}{RT^2} = \frac{34450}{T^2} - 2.01 \times \frac{1}{T}$$

$$\Delta H_{sv} = 34450 \times R - 2.01 \times RT \Big|_{T=1239}$$

$$\Delta H_{sv} = 34450 \times 8.314 - 2.01 \times 8.314 \times 1239 = 265712 \text{ J}$$

$$\Delta H_{sl} = \Delta H_{sv} - \Delta H_{lv}$$

$$\Delta H_{lv} = 31040 R - 2.52 RT \Big|_{T=1239}$$
$$= 232524 \text{ J}$$

$$\Delta H_{sl} = 265712 - 232524 = 33188 \text{ J}$$

e) $\Delta C_p = \frac{d \Delta H}{dT}$

$$\Delta H_{sl} = \Delta H_{sv} - \Delta H_{lv} = 3360 R + 0.51 RT$$

$$\frac{d \Delta H}{dT} = 0.51 R = 4.24 \text{ J/K}$$

$$\Delta C_p = 4.24 \text{ J/K}$$

$$2.) \begin{cases} dG^S = -S^S dT + V dp^S \\ - dG^L = -S^L dT + V dp^L \end{cases}$$

$$dG^{S+L} = dG_m = (S^L - S^S) dT + V (dp^S - dp^L)$$

$$dG_m = 0 \Rightarrow (S^L - S^S) dT + V_m (dp^S - dp^L) = 0$$

$$\Delta G = \Delta S = \frac{\Delta H}{T} \Rightarrow S^L - S^S = \frac{\Delta H_m}{T_m}$$

$$+ \frac{\Delta H_m}{T_m} \Delta T_m + V_m (dp^S - dp^L) = 0$$

$$dp^S - dp^L = \frac{2\gamma_L}{r} - \frac{2\gamma_S}{r}$$

$$\frac{\Delta T_m}{T_m} \times \Delta H_m + V_m \times \frac{2(\gamma_L - \gamma_S)}{r} = 0$$

$$\frac{\Delta T_m}{T_m} = \frac{\gamma_S - \gamma_L}{\Delta H_m} \times \frac{2}{r} V_m$$

$$3. G_m = x_A^0 G_A + x_B^0 G_B + RT \{ x_A \ln x_A + x_B \ln x_B \} + x_A x_B \{ L_0 + (x_A - x_B) L_1 \}$$

$$(a) G_m = x_A \bar{G}_A + x_B \bar{G}_B$$

$$dG_m = \bar{G}_A dx_A + \bar{G}_B dx_B$$

$$x_A + x_B = 1 \rightarrow dx_A = -dx_B$$

$$dG = (\bar{G}_B - \bar{G}_A) dx_B$$

$$x_A \frac{dG}{dx_B} = x_A \bar{G}_B - x_A \bar{G}_A$$

$$x_A \frac{dG}{dx_B} = x_A \bar{G}_B - G_m + x_B \bar{G}_B$$

$$\bar{G}_B = G_m + x_A \frac{dG_m}{dx_B} = G_m - x_A \frac{dG_m}{dx_A}$$

$$\bar{G}_A = G_m + x_B \frac{dG_m}{dx_A} = G_m + (1-x_A) \frac{dG_m}{dx_A}$$

$$G_m = x_A^0 G_A + (1-x_A)^0 G_B + RT \{ x_A \ln x_A + (1-x_A) \ln(1-x_A) \} + x_A(1-x_A) \{ L_0 + (2x_A-1)L_1 \}$$

$$\frac{dG_m}{dx_A} = G_A - G_B + RT \{ \ln x_A - \ln(1-x_A) \} + (1-2x_A) \{ L_0 + (2x_A-1)L_1 \} + 2L_1 x_A (1-x_A)$$

$$\bar{G}_A = G_m + (1-x_A) \frac{dG_m}{dx_A} = G_A + RT \ln x_A + (1-x_A)(1-x_A)L_0 + (1-x_A)(1-x_A)(4x_A-1)L_1$$

$$\begin{aligned} \bar{G}_B &= G_m - x_A \frac{dG_m}{dx_A} = G_B + RT \ln(1-x_A) + x_A^2 L_0 + x_A^2 (4x_A-3)L_1 \\ &= G_B + RT \ln x_B + x_A^2 L_0 + x_A^2 (-4x_B+1)L_1 \\ &= G_B + RT \ln x_B + (1-x_B^2)L_0 + (1-x_B^2)(-4x_B+1)L_1 \end{aligned}$$

$$(b) \bar{G}_A \begin{cases} \text{dilute} \text{ } x_A \rightarrow 0 \Rightarrow (1-x_A^2)L_0 + (1-x_A^2)(4x_A-1)L_1 \Big|_{x_A=0} = L_0 - L_1 : \text{Henrian 기동} \\ \text{rich} \text{ } x_A \rightarrow 1 \Rightarrow (1-x_A^2)L_0 + (1-x_A^2)(4x_A-1)L_1 \Big|_{x_A=1} = 0 : \text{Raoultian 기동} \end{cases}$$

$$\bar{G}_B \begin{cases} \text{dilute} \text{ } x_B \rightarrow 0 \Rightarrow (1-x_B^2)L_0 + (1-x_B^2)(-4x_B+1)L_1 \Big|_{x_B=0} = L_0 + L_1 : \text{Henrian 기동} \\ \text{rich} \text{ } x_B \rightarrow 1 \Rightarrow (1-x_B^2)L_0 + (1-x_B^2)(-4x_B+1)L_1 \Big|_{x_B=1} = 0 : \text{Raoultian 기동} \end{cases}$$

$$(1) \sum_i x_i d\bar{G}_i = 0$$

$$x_A d\bar{G}_A + x_B d\bar{G}_B = 0$$

$$d\bar{G}_B = -\frac{x_A}{x_B} d\bar{G}_A$$

$$\int d\bar{G}_B = \bar{G}_B = - \int \frac{x_A}{x_B} d\bar{G}_A$$

$$\bar{G}_A = {}^0\bar{G}_A + RT \ln x_A + (1-x_A)^2 L_0 + (1-x_A)(1-x_A)(4x_A-1)L_1$$

$$d\bar{G}_A = \left(\frac{1}{x_A} RT - 2(1-x_A)L_0 - 2(1-x_A)(4x_A-1)L_1 + 4(1-x_A)^2 L_1 \right) dx_A$$

$$\bar{G}_B = - \int \frac{x_A}{1-x_A} \left[\frac{1}{x_A} RT - 2(1-x_A)L_0 - 2(1-x_A)(4x_A-1)L_1 + 4(1-x_A)^2 L_1 \right] dx_A$$

$$= - \int \frac{RT}{1-x_A} - 2x_A L_0 - 2x_A(4x_A-1)L_1 + 4x_A(1-x_A)L_1 dx_A$$

$$= RT \ln(1-x_A) + x_A^2 L_0 + (4x_A^3 - 3x_A^2) \frac{L_1}{L_1} \quad C''_{G_B}$$

$$= RT \ln x_B + (1-x_B)^2 L_0 + (1-x_B)^2 (-4x_B+1)L_1 + {}^0\bar{G}_B$$

4.

$$(a) \Delta G_{(l)}^M = RT (X_A \ln X_A + X_B \ln X_B) + X_B \Delta G_m^0(B)$$

$$\Delta G_{(s)}^M = RT (X_A \ln X_A + X_B \ln X_B) - X_A \Delta G_m^0(A)$$

$$(b) \Delta G_{(l)}^M = RT (X_A \ln X_A + X_B \ln X_B)$$

$$\Delta G_{(s)}^M = RT (X_A \ln X_A + X_B \ln X_B) - X_B \Delta G_m^0(B) - X_A \Delta G_m^0(A)$$

(a)에서의 공통접선

$$\Delta G_{(l)}^M = RT (X_A \ln X_A + (1-X_A) \ln (1-X_A)) + (1-X_A) \Delta G_m^0(B)$$

$$\Delta G_{(s)}^M = RT (X_A \ln X_A + (1-X_A) \ln (1-X_A)) - X_A \Delta G_m^0(A)$$

$$\frac{d\Delta G_{(l)}^M}{dX_A} = RT \ln \frac{X_A}{1-X_A} - \Delta G_m^0(B)$$

$$\frac{d\Delta G_{(s)}^M}{dX_A} = RT \ln \frac{X_A}{1-X_A} - \Delta G_m^0(A)$$

$$\left\{ \begin{array}{l} \Delta G_{(l)}^M \text{의 } X_A = X_{A,l} \text{에서의 접선: } \left(RT \ln \frac{X_{A,l}}{1-X_{A,l}} - \Delta G_m^0(B) \right) (X_A - X_{A,l}) + \Delta G_{(l)}^M \Big|_{X_A = X_{A,l}} \\ \Delta G_{(s)}^M \text{의 } X_A = X_{A,s} \text{에서의 접선: } \left(RT \ln \frac{X_{A,s}}{1-X_{A,s}} - \Delta G_m^0(A) \right) (X_A - X_{A,s}) + \Delta G_{(s)}^M \Big|_{X_A = X_{A,s}} \end{array} \right.$$

$$RT \ln \frac{X_{A,l}}{1-X_{A,l}} - \Delta G_m^0(B) = RT \ln \frac{X_{A,s}}{1-X_{A,s}} - \Delta G_m^0(A) \quad \text{--- ①}$$

$$\left\{ \begin{array}{l} -X_{A,l} RT \ln \frac{X_{A,l}}{1-X_{A,l}} + \Delta G_m^0(B) \cdot X_{A,l} + \Delta G_{(l)}^M \Big|_{X_A = X_{A,l}} = -X_{A,s} RT \ln \frac{X_{A,s}}{1-X_{A,s}} + X_{A,s} \Delta G_m^0(B) + \Delta G_{(s)}^M \Big|_{X_A = X_{A,s}} \\ \rightarrow 2X_{A,l} RT \ln (1-X_{A,l}) + \Delta G_m^0(B) = 2X_{A,s} RT \ln (1-X_{A,s}) \quad \text{--- ②} \end{array} \right.$$

(b)에서의 공통접선

$$\Delta G_{(l)}^M \text{의 } X_A = X_{A,l2} \text{에서의 접선: } \left(RT \ln \frac{X_{A,l2}}{1-X_{A,l2}} \right) (X_A - X_{A,l2}) + \Delta G_{(l)}^M \Big|_{X_A = X_{A,l2}}$$

$$\Delta G_{(s)}^M \text{의 } X_A = X_{A,s2} \text{에서의 접선: } \left(RT \ln \frac{X_{A,s2}}{1-X_{A,s2}} + \Delta G_m^0(B) - \Delta G_m^0(A) \right) (X_A - X_{A,s2}) + \Delta G_{(s)}^M \Big|_{X_A = X_{A,s2}}$$

$$RT \ln \frac{X_{A,l2}}{1-X_{A,l2}} = RT \ln \frac{X_{A,s2}}{1-X_{A,s2}} + \Delta G_m^0(B) - \Delta G_m^0(A) \quad \text{--- ③}$$

$$-X_{A,l2} RT \ln \frac{X_{A,l2}}{1-X_{A,l2}} + \Delta G_m^M \Big|_{X_A=X_{A,l2}} = -X_{A,s2} RT \ln \frac{X_{A,s2}}{1-X_{A,s2}} - X_{A,s2} \Delta G_m^0 + X_{A,s2} \Delta G_{m(P)}^0 + \Delta G_{(s)}^M \Big|_{X_A=X_{A,s2}}$$

$$2X_{A,l2} RT \ln(1-X_{A,l2}) = 2X_{A,s2} RT \ln(1-X_{A,s2}) - \Delta G_m^0(R) - (4)$$

①식과 ③번식이, ②식과 ④식이 같다.

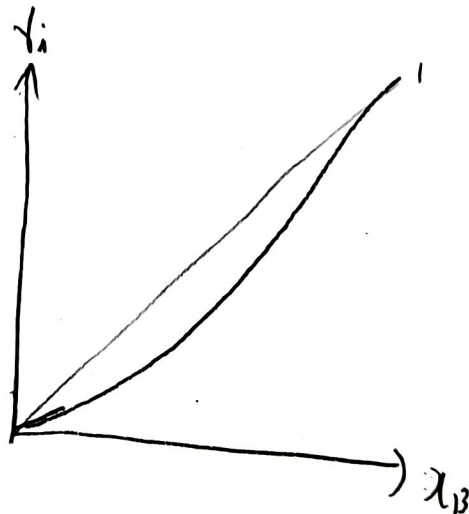
따라서 ~~(1)번식~~ $X_{A,l} = X_{A,l2}$ & $X_{A,s} = X_{A,s2}$

∴ 상평형 조성은 둘이 같다.

5.

$$\gamma_i = \frac{a_B}{X_B}$$

x_B	a_B	γ_i
0.1	0.0320	0.3200
0.2	0.0800	0.4000
0.3	0.1448	0.4993
0.4	0.2400	0.6000
0.5	0.3510	0.7020
0.6	0.4782	0.7970
0.7	0.6162	0.8803
0.8	0.7559	0.9449
0.9	0.8874	0.9860
1.0	1.0000	1.0000



ideal 한 경우 $\gamma_i = 1$ 이어야 하는데 그렇지 않다.

regular model 인 경우 $\frac{\ln \gamma_i}{(1-x_i)^2}$ 가 일정해야 한다.

x_B	γ_i	$\frac{\ln \gamma_i}{(1-x_B)^2}$
0.1	0.3200	-1.4067
0.2	0.4000	-1.4317
0.3	0.4943	-1.4173
0.4	0.6000	-1.4190
0.5	0.7020	-1.4153
0.6	0.7470	-1.4181
0.7	0.8803	-1.4168
0.8	0.9449	-1.4176
0.9	0.9860	-1.4099
1	1	

$$\frac{\ln \gamma_i}{(1-x_B)^2} = a_i \text{ 는 거의 일정하다}$$

∴ 성분 B는 regular 모델을 따른다.

Molar Gibbs Energy of mixing $\bar{G}_B = RT x_B \ln a_B$

$$\frac{\ln \gamma_i}{(1-x_B)^2} = a \approx -1.4164$$

$$\ln \frac{a_i}{x_B} = a(1-x_B)^2$$

$$a_i = x_B e^{a(1-x_B)^2} = x_B e^{-1.4164(1-x_B)^2}$$

x_B	a_i 수식
0.1	0.0317
0.2	0.0808
0.3	0.1498
0.4	0.2402
0.5	0.3509
0.6	0.4783
0.7	0.6162
0.8	0.7559
0.9	0.8873
1	1

수식으로 계산한 것과 실험 데이터와의 차이가 거의 없다.

Sub regular model은 3번째 문제에서 구한 식을 이용한다.

$$\bar{G}_B = G_B + RT \ln x_B + (1-x_B^2)L_0 + (1-x_B^2)(1-4x_B)L_1$$

$$RT \ln a_B = (RT \ln x_B + (1-x_B^2)L_0 + (1-x_B^2)(1-4x_B)L_1)$$

$$L_0, L_1 \text{을 구하기 위해 } \begin{pmatrix} x_B=0.1 & a_B=0.032 \\ x_B=0.2 & a_B=0.08 \end{pmatrix} \text{ 대입}$$

$$8.314 \times 1273 \times \ln 0.032 = 8.314 \times 1273 \times \ln 0.1 + (1-0.1^2)L_0 + (1-0.1^2)(1-4 \times 0.1)L_1$$

$$-36429 = -24370 + 0.99L_0 + 0.594L_1$$

$$0.99L_0 + 0.594L_1 = -12059$$

$$8.314 \times 1273 \times \ln 0.08 = 8.314 \times 1273 \times \ln 0.2 + (1-0.2^2)L_0 + (1-0.2^2)(1-4 \times 0.2)L_1$$

$$-26732 = -17034 + 0.84L_0 + 0.192L_1$$

$$0.84L_0 + 0.192L_1 = -9698$$

$$L_0 = -11154 \quad L_1 = -1711$$

이를 통해 a_B 값을 구해보면

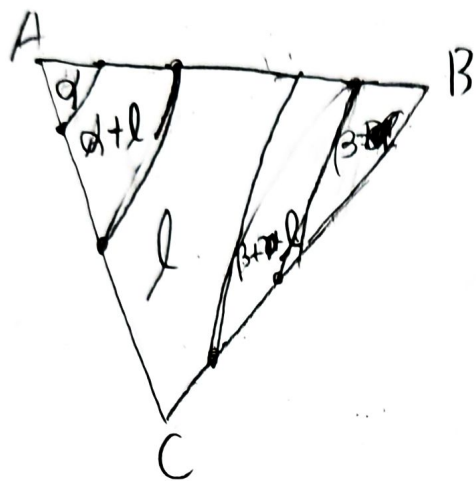
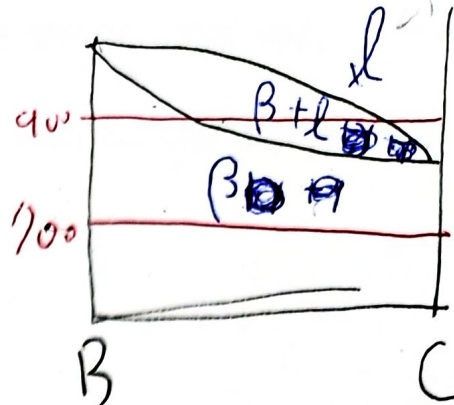
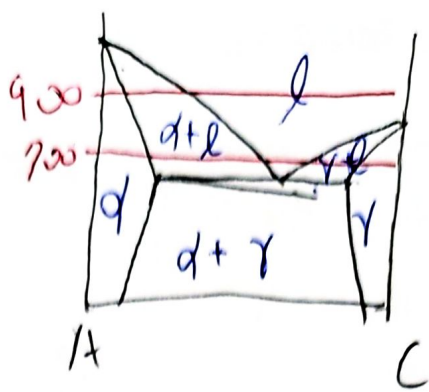
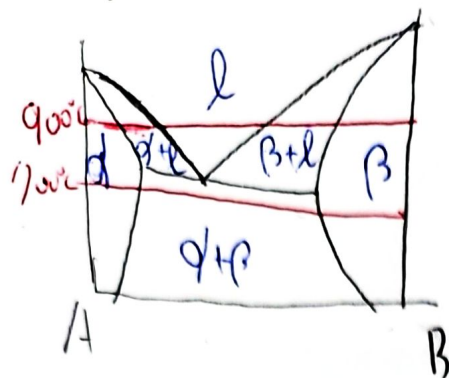
$$a_B = \exp \left\{ \ln x_B + \frac{(1-x_B^2) \times (-11154) - (1-x_B^2)(1-4x_B) \times (-1711)}{RT} \right\}$$

x_B	a_B
0.1	0.032
0.2	0.08
0.3	0.1184
0.4	0.1791
0.5	0.2561
0.6	0.3533
0.7	0.4744
0.8	0.6222
0.9	0.7979
1.0	1

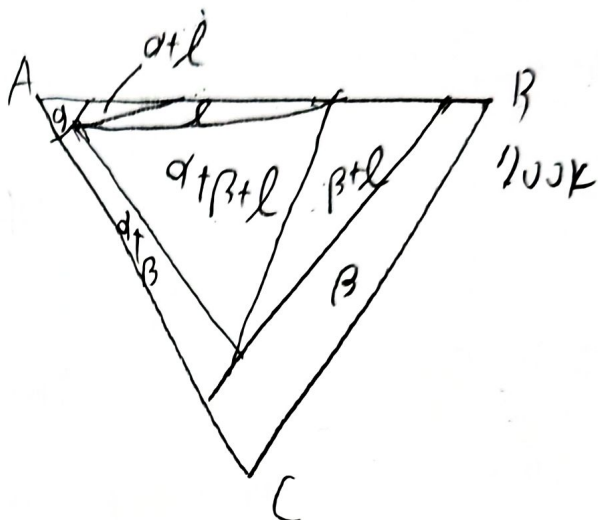
수식으로 계산한 것과 실험 데이터와의 차이가 크다.

$\therefore$ regular 모델을 따른다고 볼 수 없다.

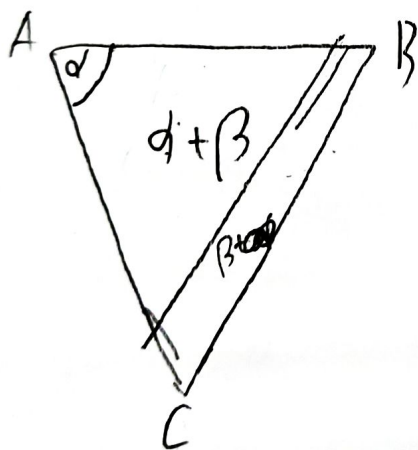
6.



900/L



700/L



400/L