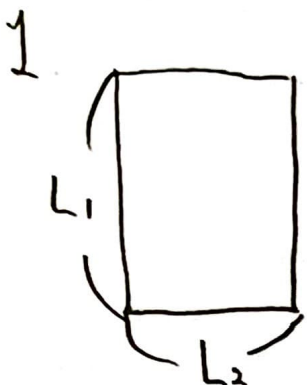


20220735 김주영.



$$A := L_1 L_2 \text{ (constant)}$$

$U :=$ 결장의 총 표면 자유에너지

$$U = \int \gamma dl = 2 \int_0^{L_1} \gamma_1 dl + 2 \int_0^{L_2} \gamma_2 dl$$

$$= 2\gamma_1 L_1 + 2\gamma_2 L_2$$

$$= 2\gamma_1 L_1 + 2\gamma_2 \frac{A}{L_1}$$

$$\frac{\partial U}{\partial L_1} = 2\gamma_1 - 2\gamma_2 \frac{A}{L_1^2} = 0 \text{ 일때 } U \text{ 가 최소가 된다.}$$

양변에 L_1 을 곱해주면 $2\gamma_1 L_1 - 2\gamma_2 \frac{A}{L_1} = 0$

$$2\gamma_1 L_1 - 2\gamma_2 L_2 = 0$$

$$\therefore \frac{L_1}{L_2} = \frac{\gamma_2}{\gamma_1} \text{ 일때 } U \text{ 가 최소가 된다.}$$

2.

$$Z = \sum_{\text{state}} e^{-\epsilon_z/kT}, \quad \epsilon_z = \frac{h^2}{8m} \left(\frac{n_x^2}{a^2} + \frac{n_y^2}{b^2} \right)$$

$$= \sum e^{-(h^2/8mkT)(n_x^2/a^2)} \sum e^{-(h^2/8mkT)(n_y^2/b^2)}$$

$$= \int_0^\infty e^{-(h^2/8mkT)(n_x^2/a^2)} dn_x \int_0^\infty e^{-(h^2/8mkT)(n_y^2/b^2)} dn_y$$

$$= \left[\frac{a}{2} \sqrt{\frac{8\pi mkT}{h^2}} \right] \left[\frac{b}{2} \sqrt{\frac{8\pi mkT}{h^2}} \right] = \frac{ab}{4} \cdot \frac{8\pi mkT}{h^2}$$

$$= A \cdot \frac{2\pi mkT}{h^2}$$

$$\int_0^\infty e^{-ax^2} dx = \frac{1}{2} \sqrt{\frac{\pi}{a}}$$

$$\ln Z = \ln A + \ln T + \ln \frac{2\pi mkT}{h^2}$$

$$P = NkT \left(\frac{\partial \ln Z}{\partial A} \right) = NkT \cdot \frac{1}{A} \equiv \frac{nRT}{A}$$

$$\Rightarrow PA = nRT$$

$$U = NkT^2 \left(\frac{\partial \ln Z}{\partial T} \right) = NkT^2 \cdot \frac{1}{T} = NkT$$

3.

$$Z = \sum_{\text{state}} e^{-\epsilon_i/kT} = e^{-0/kT} + e^{-\epsilon/kT} \quad (\text{이웃한 분자 2개에 대하여})$$

$$= 1 + e^{-\epsilon/kT}$$

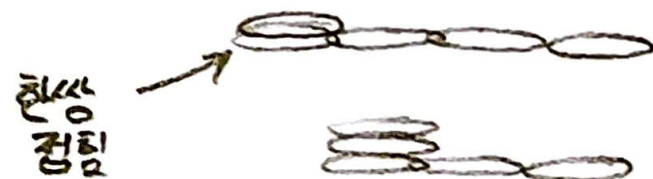
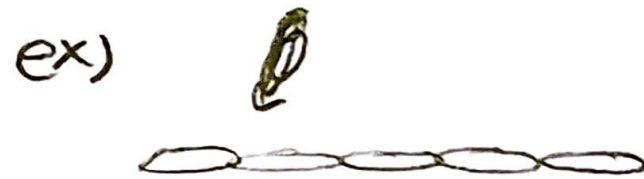
$$\text{완전히 고정된 확률: } \frac{e^{-\epsilon/kT}}{1 + e^{-\epsilon/kT}}$$

$$\text{안고쳐질 확률: } \frac{1}{1 + e^{-\epsilon/kT}} \quad \text{찍이는 관절수}$$

$$\text{평균적으로 완전히 고정되는 이웃한 분자쌍의 수: } (N-1) \frac{e^{-\epsilon/kT}}{1 + e^{-\epsilon/kT}}$$

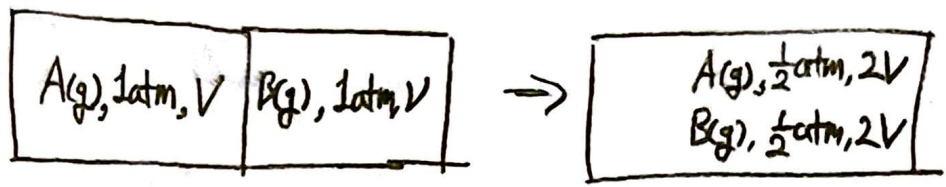
$$x \text{ 쌍이 접리면 분자전체 길이는 } Na - xa = (N-x)a$$

$$\therefore \left[\left(N - (N-1) \frac{e^{-\epsilon/kT}}{1 + e^{-\epsilon/kT}} \right) a \right]$$



~~N개의~~ N개의 분자가 있고
N-1개의 이웃한 분자쌍이
있음.

4.



~~$S = k_B \ln \Omega$~~

(a)

$$\Delta S'_{\text{conf}} = -k(N_A + N_B) [X_A \ln X_A + X_B \ln X_B]$$

$$= -2R \left(\frac{1}{2} \ln \frac{1}{2} + \frac{1}{2} \ln \frac{1}{2} \right) = R \ln 4 \quad \left(k = \frac{R}{N_A} \right)$$

(b)

$$\Delta S_{\text{config}} = k \ln \left(\frac{3N_A!}{2N_A! \cdot N_A!} \right) \approx k (3N_A \ln 3N_A - 3N - 2N_A \ln 2N_A + 2N_A - N_A \ln N_A + N_A)$$

$$= 3R \ln 3N_A - 2R \ln 2N_A - R \ln N_A$$

$$= R \left(\ln \frac{27}{4} \right)$$

$$\Delta S_{\text{thermal}, A} = nR \ln \left(\frac{V_2}{V_1} \right) = 2R \ln \frac{4}{3}$$

$$\Delta S_{\text{thermal}, B} = nR \ln \left(\frac{V_2}{V_1} \right) = R \ln \frac{2}{3}$$

$$\Delta S_{\text{total}} = R \ln \frac{27}{4} + R \ln \frac{16}{9} + R \ln \frac{2}{3} = R \ln 8$$

(c)

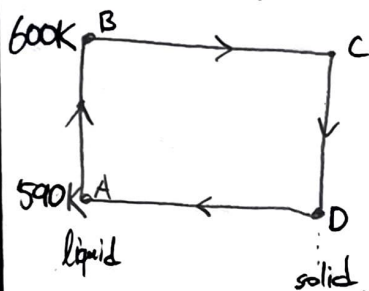
(a)에 대해서는 $\Delta S_{\text{thermal}} = 0$ (부피변화 X), $\Delta S_{\text{config}} = k \left(\ln \frac{2N_A!}{2N_A!} \right) = 0$
 $\Delta S_{\text{total}} = 0$

(b)에 대해서는 $\Delta S_{\text{thermal}, A1} = nR \ln \left(\frac{V_2}{V_1} \right) = 2R \ln \left(\frac{\frac{2}{3}V}{\frac{1}{2}V} \right) = 2R \ln \frac{4}{3}$
 $\Delta S_{\text{thermal}, A2} = R \ln \left(\frac{\frac{1}{3}}{\frac{1}{2}} \right) = R \ln \frac{2}{3}$
 $\Delta S_{\text{config}} = k \left(\ln \frac{3N_A!}{3N_A!} \right) = 0$

$$\Delta S_{\text{total}} = 2R \ln \frac{4}{3} + R \ln \frac{2}{3} = R \ln \frac{32}{27}$$

#5.

(1) maximum entropy criterion.



$n = 1 \text{ mol}$ 3.75g

$$\Delta S_{A \rightarrow D} = \Delta S_{A \rightarrow B} + \Delta S_{B \rightarrow C} + \Delta S_{C \rightarrow D}$$

$$\Delta S_{A \rightarrow B} = \int_{590K}^{600K} \frac{n C_{p(l)}}{T} dT = \int_{590K}^{600K} \left(\frac{32.4}{T} - 3.1 \times 10^{-3} \right) dT = \left(32.4 \ln \frac{600K}{590K} - 3.1 \times 10^{-3} (600K - 590K) \right) \text{ J/K}$$

$$= 0.51 \text{ J/K}$$

$$\Delta S_{B \rightarrow C} = \frac{\Delta Q}{T} = \frac{-n \Delta H_m}{T} \quad (\because \text{등압 조건에서 가열}) = \frac{-4810 \text{ J}}{600K} = -8.02 \text{ J/K} \quad (\Delta H_{\text{fuz}} = -\Delta H_m)$$

$$\Delta S_{C \rightarrow D} = \int_{600K}^{590K} \frac{n C_{p(s)}}{T} dT = 9.75 \times 10^{-3} (590K - 600K) = -0.10 \text{ J/K}$$

$$\Delta S_{A \rightarrow D} = -7.61 \text{ J/K} \quad \text{which is } \Delta S_{\text{sys}}$$

$$\Delta S_{\text{sur}} = -\frac{\Delta H_{A \rightarrow D}}{T}$$

$$\Delta H_{A \rightarrow B} = \int_{590K}^{600K} n C_{p(l)} dT = \int_{590K}^{600K} (32.4 - 3.1 \times 10^{-3} T) dT = 32.4(600K - 590K) - \frac{1}{2}(3.1 \times 10^{-3})(600^2 - 590^2) = 306 \text{ J}$$

$$\Delta H_{B \rightarrow C} = -n \Delta H_m = -4810 \text{ J}$$

$$\Delta H_{C \rightarrow D} = \int_{600}^{590} n C_{p(s)} dT = \frac{1}{2}(9.75 \times 10^{-3})(590^2 - 600^2) = -58.0 \text{ J}$$

$$\Delta H_{A \rightarrow D} = -4562 \text{ J}$$

$$\Delta S_{\text{sur}} = -\frac{\Delta H_{A \rightarrow D}}{T} = \frac{4562}{590} = 7.73 \text{ J/K}$$

$$-4810 =$$

$$\Delta S_{\text{total}} = \Delta S_{\text{sys}} + \Delta S_{\text{sur}} = 0.12 \text{ J/K} > 0 \Rightarrow \text{자발적}$$

$$\int_{590}^{T_2} C_{p(s)} dT$$

(2)

$$\Delta G = \Delta H - T \Delta S = \Delta H_{A \rightarrow D} - T \Delta S_{A \rightarrow D} = -4562 - 590 \times (-7.61) = -72.1 \text{ J} < 0 \Rightarrow \text{자발적}$$

단일상태였다면 응고하며 생성된 열이 system을 빠져나가지 못해 고체의 일부는 다시 녹는다.

$n = 1 \text{ mol}$ 중에 x 의 몰만큼 응고된다고 해보면, adiabatic 과정이므로 $\Delta H = \Delta H_{A \rightarrow B} + \Delta H_{B \rightarrow C} = 0$

$$\Delta H_{A \rightarrow B} = \int_{590}^{600} n C_{p(l)} dT = 306 \text{ J} \quad (\text{앞에서 구함})$$

$$\Delta H_{B \rightarrow C} = -x \Delta H_m = -4810x \text{ J}$$

$$x = \frac{306}{4810} = 0.06 \quad \text{따라서}$$

0.04 몰만큼 액상으로, 0.06 몰만큼 고상으로 존재한다.

응고될 때 방출된 엔탈피는 4810J 이지만 $\Delta H_m = 4810$ 이고, 실제로 4562 중에 일부는 온도변화에 사용되므로 최종엔도는 melting point에 걸리게 된다.

600K의 액상 60여%의 고상 등하게 존재

< 고체와 액체가 공존한 거라

생각한 이유

#6

 $n = 1$ 몰이라고 가정하라

25°C 1기압에서

$$\Delta G = \Delta H - T \Delta S = 454 - 298(0.58 - 1.37) = 689 \text{ J} > 0 \text{로 비자발적이다.}$$

1기압에서 P_0 기압으로 바뀌면,

$$\Delta H_{298, 1 \rightarrow P_0}(\text{graphite}) = \int_1^{P_0} V_g(1 - \alpha_g T) dP = V_g(1 - \alpha_g T)(P_0 - 1)$$

$$\Delta H_{298, 1 \rightarrow P_0}(\text{diamond}) = \int_1^{P_0} V_d(1 - \alpha_d T) dP = V_d(1 - \alpha_d T)(P_0 - 1)$$

따라서 P_0 압력에서 몰엔탈피의 차이는

$$-454 + V_g(1 - \alpha_g T)(P_0 - 1) - V_d(1 - \alpha_d T)(P_0 - 1) \text{ 이다.}$$

$$= -\Delta H_{\text{new}}$$

 P_0 압력에서 엔트로피의 차이를 구해보면

$$S_{298, P_0}(\text{graphite}) = 1.37 - \int_1^{P_0} \alpha_g V_g dP = 1.37 - \alpha_g V_g(P_0 - 1), S_{298, P_0}(\text{diamond}) = 0.58 - \int_1^{P_0} \alpha_d V_d dP = 0.58 - \alpha_d V_d(P_0 - 1)$$

$$\Delta S_{\text{new}} = S_{298, P_0}(\text{diamond}) - S_{298, P_0}(\text{graphite}) = -0.79 + \alpha_g V_g(P_0 - 1) - \alpha_d V_d(P_0 - 1)$$

$$\Delta G_{\text{new}} = \Delta H + T \Delta S = (P_0 - 1) \{ V_d(1 - \alpha_d T) - V_g(1 - \alpha_g T) + \alpha_g V_g T - \alpha_d V_d T \} + 218.6$$

$$= \Delta H_{\text{new}} + T \Delta S_{\text{new}}$$

$$= (P_0 - 1)(V_d - V_g) + 218.6 \text{ cal} = (P_0 - 1)(V_d - V_g) + 9.03 \text{ atm} \cdot \text{L}$$

 $\Delta G < 0$ 이면 자발적이므로 $P_0 > -\frac{9.03}{V_d - V_g} + 1$ ($V_d < V_g$) 인 P_0 를 압력으로 설정하면 반응이 일어난다.

$$V_g = 0.0053 \text{ L} \left(\frac{1}{2.22} \times 12 \times 10^{-3} (\text{L/cm}^3) \right)$$

$$V_d = 0.0034 \text{ L} \left(\frac{1}{3.55} \times 12 \times 10^{-3} (\text{L/cm}^3) \right)$$

$$P_0 > 4753 (\text{atm}) \text{ 일때 반응이 일어난다.}$$