

REPORT



POSTECH

POHANG UNIVERSITY OF SCIENCE AND TECHNOLOGY

제목 : Homework #6

수강과목 : 상변태론

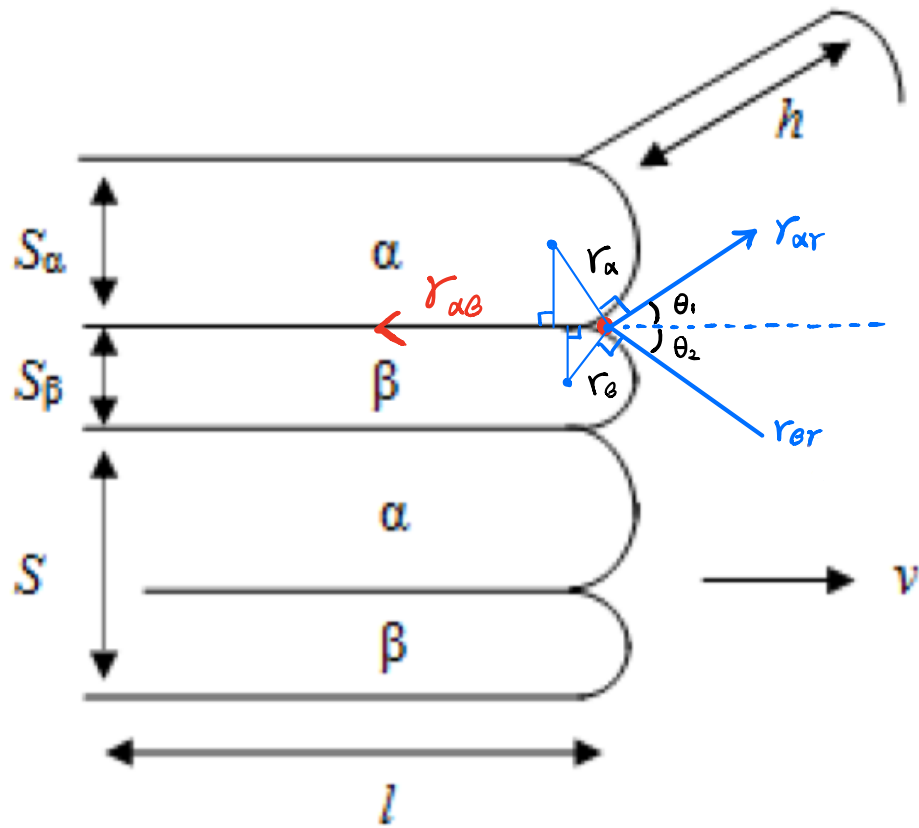
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1. (a)

α - phase 와 β - phase 사이의 interface energy γ_{ab} 가 두 평형식을 만족

$$\left\{ \begin{array}{l} \gamma_{ab} = \gamma_{\alpha r} \cos \theta_1 + \gamma_{\beta r} \cos \theta_2 \quad - (1) \\ \gamma_{\alpha r} \sin \theta_1 = \gamma_{\beta r} \sin \theta_2 \quad - (2) \end{array} \right.$$

Tip 이 Curvature 를 가지지 않는다면, $\theta_1 = \theta_2 = 90^\circ$ 이고

$\gamma_{ab} = 0$ 인데, surface energy 가 0 인 interface 가 존재할 수 없다.

따라서, 가정이 틀렸음을 알 수 있고 tip 은 Curvature 를 가져야 한다.

1. (b) ② 식을 통해 θ_2 를 θ_1 에 대해 나타내면

$$\gamma_{\alpha r}^2 \sin^2 \theta_1 = \gamma_{\alpha r} (1 - \cos^2 \theta_1) = \gamma_{\beta r}^2 (1 - \cos^2 \theta_2)$$

$$\cos \theta_2 = \left(\frac{\gamma_{\beta r}^2 - \gamma_{\alpha r}^2 + \gamma_{\alpha r}^2 \cos^2 \theta_1}{\gamma_{\beta r}^2} \right)^{\frac{1}{2}} \text{ 로 나타낼 수 있고}$$

$$\textcircled{1} \text{ 식은 } r_{AB} = r_{Ar} \cos \theta_1 + \cancel{r_{Br}} \left(\frac{r_{Br}^2 - r_{Ar}^2 + r_{Ar}^2 \cos^2 \theta_1}{\cancel{r_{Br}^2}} \right)^{\frac{1}{2}} \quad \textcircled{3}$$

Curvature radius r_a 이 r_b 에 대해,

$$S_a = 2r_a \cos \theta_1, \quad S_b = 2r_b \cos \theta_2 \quad \text{를 만족한다. 이들을 식 } \textcircled{3} \text{ 에 적용}$$

$$r_{AB} = r_{Ar} \frac{S_a}{2r_a} + \sqrt{r_{Br}^2 - r_{Ar}^2 + r_{Ar}^2 \frac{S_a^2}{4r_a^2}}$$

$$\left(r_{AB} - r_{Ar} \frac{S_a}{2r_a} \right)^2 = r_{Br}^2 - r_{Ar}^2 + r_{Ar}^2 \frac{S_a^2}{4r_a^2}$$

$$r_{AB}^2 - \frac{r_{AB} \cdot r_{Ar} \cdot S_a}{r_a} + \frac{\cancel{r_{Ar}^2 S_a^2}}{4r_a^2} = r_{Br}^2 + r_{Ar}^2 + \cancel{r_{Ar}^2 \frac{S_a^2}{4r_a^2}}$$

$$\therefore r_a = \frac{S_a r_{AB} r_{Ar}}{r_{AB}^2 - r_{Br}^2 + r_{Ar}^2}, \quad r_b = \frac{S_b r_{AB} r_{Br}}{r_{AB}^2 - r_{Ar}^2 + r_{Br}^2}$$

(c) Capillary effect에 의한 Gibbs free energy increase ΔG

$$\Delta G = \frac{r_{Ar}}{r_a} V_a + \frac{r_{Br}}{r_b} V_b \quad (\text{cylinder 에서 Capillary effect})$$

(b) 의 결과를 적용하면,

$$\Delta G = \frac{\cancel{r_{Ar}}(r_{AB}^2 - r_{Br}^2 + r_{Ar}^2)}{S_a r_{AB} \cancel{r_{Ar}}} V_a + \frac{\cancel{r_{Br}}(r_{AB}^2 - r_{Ar}^2 + r_{Br}^2)}{S_b r_{AB} \cancel{r_{Br}}} V_b$$

$$\frac{V_a}{S_a} = \frac{V_b}{S_b} = \frac{V_m}{S} \quad \text{이라고 하면.} \quad \Delta G = \frac{V_m}{S} \left(\frac{2r_{AB}^2}{r_{AB}} \right) = \frac{2r_{AB} V_m}{S}$$

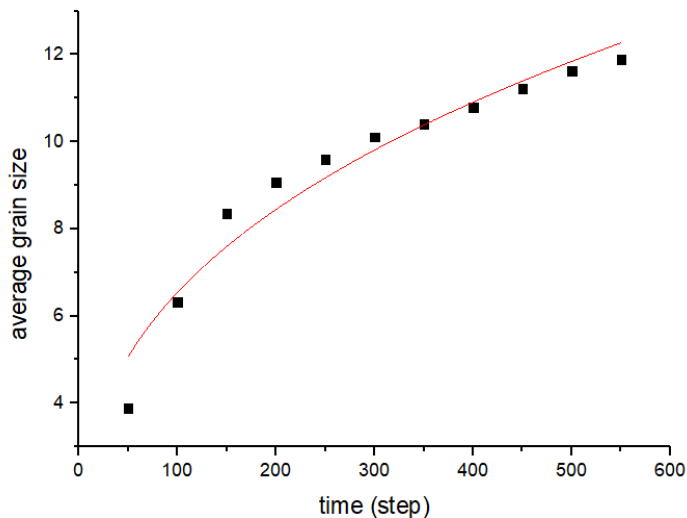
2(a) Set:

- Initial 64000 grain,
- 10 temperature
- 50 step as time goes on

The average grain size can be represented

$$R = Kt^n$$

$$n = 0.36919, k = 1.722 - (a)$$



Equation	a*x^b		
Reduced Chi-Sqr	0.32495		
Adj. R-Square	0.94491		
		Value	Standard Error
average grain size	a	1.19424	0.22987
	b	0.36919	0.03292

2(b) Set: Initial 64000 grain,
200 step at each temperature(1~20)

$$R = Kt^n$$

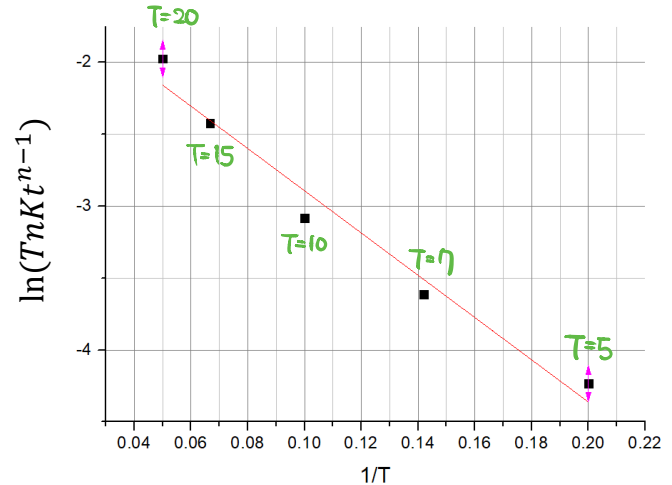
$$\frac{dR}{dt} = nKt^{n-1} = \lambda V$$

$$V = V_0 e^{-\frac{\Delta G^*}{RT}} (1 - e^{-\frac{\Delta G_{eff}}{RT}}) = V_0 e^{-\frac{\Delta G^*}{RT}} \frac{\Delta G_{eff}}{RT} \quad (\Delta G_{eff} \ll RT)$$

$$nKt^{n-1} = \lambda V_0 e^{-\frac{\Delta G^*}{RT}} \frac{\Delta G_{eff}}{RT} \quad (C = \frac{\lambda V_0 \Delta G_{eff}}{R})$$

$$\therefore \Rightarrow \ln(TnKt^{n-1}) = \ln C - \frac{\Delta G^*}{RT} \quad (b) - ①$$

$$\begin{aligned} \therefore \Delta G^* &= (\text{slope}) \times R = (14.69) \times (8.314) \\ &= 122.13 \quad (b) - ② \end{aligned}$$



Equation	y = a + b*x		
Weight	No Weighting		
Residual Sum of Squares	0.09789		
Pearson's r	-0.98491		
Adj. R-Square	0.96005		
		Value	Standard Error
B	Intercept	-1.42448	0.1851
	Slope	-14.69068	1.49056