

1.

$$P_i = 10 \text{ atm}, \quad T_i = 300 \text{ K} \quad P_f = 5 \text{ atm} \quad n = 1$$

$$P_i V_i = nRT_i \quad V_i = 2.462 \text{ L}$$

(a) isothermal

$$P_i V_i = P_f V_f \quad \therefore V_f = \frac{P_i}{P_f} V_i = 4.924 \text{ L}$$

$$\Delta T = 0 \Rightarrow \Delta U = 0 \Rightarrow q = W$$

$$W = \int_{2.462}^{4.924} \frac{nRT}{V} dV = nRT \ln 2 = 1.728 \text{ kJ} = q$$

$$\Delta S = \frac{q}{T} = 5.763 \text{ J/K}$$

(b) reversible adiabatic

$$\text{monatomic} \Rightarrow C_v = \frac{3}{2}R, \quad C_p = \frac{5}{2}R, \quad \gamma = \frac{5}{3}$$

$$P_i V_i^\gamma = P_f V_f^\gamma \quad V_f = V_i \cdot \left(\frac{P_i}{P_f}\right)^{1/\gamma} = 3.732 \text{ L} \dots \text{ ok...}$$

$$q = 0 \quad \text{or} \quad \Delta S = \frac{q}{T} = 0$$

(c) Constant-volume

$$\Delta U = q \quad (\because W = 0)$$

$$P_f V_f = nRT_f \Rightarrow T_f = \frac{P_f V_f}{nR} = 150 \text{ K}$$

$$\Delta S = \frac{q}{T} = \frac{\Delta U}{T} = \int_{300}^{150} \frac{nC_v}{T} dT = C_v \cdot \ln \frac{1}{2} = -8.645 \text{ J/K}$$

2.

 $n=1$, monoatomic ideal gas

$$a. T_o = 300 \text{ K}, P_o = 10 \text{ atm} \Rightarrow V_o = 2.462 \text{ L}$$

$$\text{expands freely} \quad C_v = \frac{3}{2}R, C_p = \frac{5}{2}R, \gamma = \frac{5}{3}, V_a = 3V_o$$

$$P_o V_o^\gamma = P_a V_a^\gamma \quad P_a = P_o \left(\frac{V_o}{V_a} \right)^\gamma = 10 \cdot \left(\frac{1}{3} \right)^{\frac{5}{3}} = 1.602 \text{ atm}$$

$$T_a = \frac{P_a V_a}{nR} = 144.24 \text{ K}$$

$$\Delta U_a = \int_{300}^{144.24} C_v dT = -1.942 \text{ kJ}, \quad \Delta H_a = \int_{300}^{144.24} C_p dT = -3.238 \text{ kJ}$$

$$\Delta S_a = 0 \quad (\because \text{adiabatic process} \Rightarrow q=0)$$

$$q_a = 0, \quad w_a = -\Delta U_a = 1.942 \text{ kJ}$$

$$b. V_a = V_b, T_b = 400 \quad \text{constant volume}$$

$$P_b = \frac{nRT_b}{V_b} = 4.444 \text{ atm}$$

$$\Delta U_b = \int_{144.24}^{400} C_v dT = 3.190 \text{ kJ}, \quad \Delta H_b = \int_{144.24}^{400} C_p dT = 5.316 \text{ kJ}$$

$$\Delta S_b = \int_{144.24}^{400} \frac{C_v}{T} dT = C_v \ln \frac{400}{144.24} = 12.72 \text{ J/K}$$

$$w_b = 0 \quad (\because \Delta V = 0) \quad q_b = \Delta U_b = 3.190 \text{ kJ}$$

C isothermal $V_c = V_b \times 3 = 7.386 \times 3 = 22.16 \text{ L}$

$$P_b V_b = P_c V_c \Rightarrow P_c = \frac{P_b V_b}{V_c} = 1.481 \text{ atm}$$

$$\Delta U_c = \Delta H_c = 0 \quad (\because dT=0)$$

$$\Delta S_c = \frac{q}{T} = \frac{w}{T} = \frac{1}{T} \int_{7.358}^{22.16} \frac{RT}{V} dV = R \ln 3 = 9.134 \text{ J/K}$$

$$q_c = w_c = 3.654 \text{ kJ}$$

d. constant pressure. $T_d = 300$

$$V_d = \frac{nRT_d}{P_d} = 16.62 \text{ L}$$

$$\Delta U_d = \int_{400}^{300} C_v dT = -1.247 \text{ kJ} \quad \Delta H_d = \int_{400}^{300} C_p dT = -2.079 \text{ kJ}$$

$$\Delta S_d = \int_{400}^{300} \frac{C_p}{T} dT = C_p \ln \frac{3}{4} = -5.980 \text{ J/K}$$

$$w_d = P \Delta V = 5.99 \text{ L} \times 1.481 \text{ atm} \times 0.1325 \text{ J/L} \cdot \text{atm} = -0.899 \text{ kJ}$$

$$q_d = \Delta U_d + w_d = -2.146 \text{ kJ}$$

$$q = q_a + q_b + q_c + q_d = (0 + 3.190 + 3.654 - 2.146) \text{ kJ} = 4.698 \text{ kJ}$$

$$w = w_a + w_b + w_c + w_d = (1.942 + 0 + 3.654 - 0.899) \text{ kJ} = 4.697 \text{ kJ}$$

$$\Delta U = \Delta U_a + \Delta U_b + \Delta U_c + \Delta U_d = (-1.942 + 3.190 + 0 - 1.247) \text{ kJ} = 0.001 \text{ kJ}$$

$$\Delta H = \Delta H_a + \Delta H_b + \Delta H_c + \Delta H_d = (-3.238 + 5.316 + 0 - 2.079) \text{ kJ} = -0.001 \text{ kJ}$$

$$\Delta S = \Delta S_a + \Delta S_b + \Delta S_c + \Delta S_d = (0 + 12.72 + 9.134 - 5.980) \text{ J/K} = 15.874 \text{ J/K}$$

3.

$$Z = (x-2)^2 + (y-2)^2 + 4 =: f(x, y)$$

$$g(x, y) := x + y - 1 = 0$$

$$\nabla f = (2x-4, 2y-4)$$

$$\nabla g = (1, 1)$$

extreme point $\hat{=}$ (a, b) 라 하면

$$\begin{cases} a+b-1=0 \\ (2a-4, 2b-4) = \lambda(1, 1) \end{cases}$$

$$\begin{cases} a+b=1 \\ 2a=\lambda+4 \\ 2b=\lambda+4 \end{cases} \rightarrow \lambda = -3, \quad a=b=\frac{1}{2}$$

$$\therefore \text{extreme value} = f\left(\frac{1}{2}, \frac{1}{2}\right) = \frac{17}{2}$$

4.

$$\Delta S_{\text{total}} = \Delta S_{\text{configuration}} \quad (\text{No chemical reaction})$$

$$(a) \quad \Omega_{\text{divided}} = \frac{N_A!}{0! N_A!} \cdot \frac{N_A!}{0! N_A!} = 1$$

partition 이 재배된 $\rightarrow$ most probable 한 state는 반반씩 섞이는 것이다.

N_A 는 매우 크므로 $\Omega_{\text{mixed}} \approx \Omega(A, B \text{ 반반 섞임})$ 이다.

$$\Rightarrow \Omega_{\text{mixed}} = \frac{(2N_A)!}{N_A! N_A!}, \quad \ln(x!) \approx x \ln x - x$$

$$\Delta S_{\text{conf}} = k_B \ln \frac{\Omega_{\text{mixed}}}{\Omega_{\text{divided}}} = k_B (2N_A \ln(2N_A) - 2N_A \ln N_A) = 11.53 \text{ J/K}$$

$$(b) \Omega_{\text{divided}} = \frac{(2N_A)!}{0! (2N_A)!} \cdot \frac{N_A!}{0! N_A!} = 1$$

(a) 이식과 마찰가리드 반씩 있을 때가 most probable하며, N_A 가 크므로 $\Omega_{\text{mixed}} \approx \Omega(A, B \text{ 반반})$ 이 성립한다.

$$\Rightarrow \Omega_{\text{mixed}} = \frac{(2N_A)!}{N_A! N_A!} \cdot \frac{N_A!}{(\frac{N_A}{2})! (\frac{N_A}{2})!}$$

$$\therefore \Delta S_{\text{tot}} = k_B \ln \frac{\Omega_{\text{mixed}}}{\Omega_{\text{divided}}} = k_B \ln \Omega_{\text{mixed}}$$

$$= k_B \left(2N_A \ln(2N_A) - \cancel{2N_A} - 2N_A \ln N_A + \cancel{2N_A} + N_A \ln N_A - N_A \ln \frac{N_A}{2} \right)$$

$$= 17.29 \text{ J/K}$$

(c) 두 part 는 ideal gas A를 가하므로 indistinguishable

$$\Rightarrow \Delta S = \Delta S_{\text{conf}} = 0$$

(d) St state function 이므로 left part 와 right part 의 압력은 같은 후 partition 을 치면 같은 것 이다.

2atm	1atm	$\rightarrow$	$\frac{4}{3}V, \frac{3}{2}\text{atm}$	$\frac{2}{3}V,$
V	V			$\frac{3}{2}\text{atm}$

$$\Delta S = \frac{PdV}{T} = \frac{1}{T} \left(\int_V^{\frac{4}{3}V} \frac{2RT}{V} dV + \int_V^{\frac{2}{3}V} \frac{RT}{V} dV \right)$$

$$= 2R \ln \frac{4}{3} + R \ln \frac{2}{3} = 1.413 \text{ J/K}$$

partition 치는 후 양 part 의 Pressure 는 같으므로 (c) 이 때의 partition 에게의 $\Delta S = 0$

$$\Rightarrow \Delta S_{\text{tot}} = 1.413 \text{ J/K}$$